

Properties of the transmission line matrix model for outdoor sound propagation: Numerical dispersion effects

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Journées techniques acoustique et vibrations
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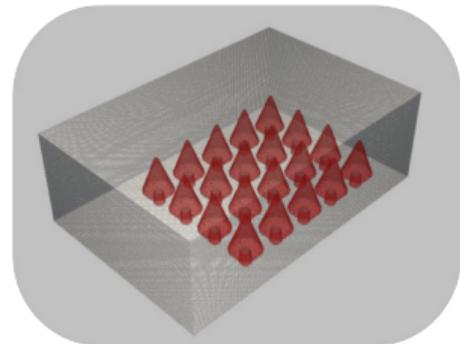
²UMRAE, Univ Gustave Eiffel, CEREMA, F-44344 Bouguenais, France

- Introduction & context
- *Transmission Line Matrix* (TLM) numerical model
- Numerical experiments
- Results
- Conclusion & perspectives

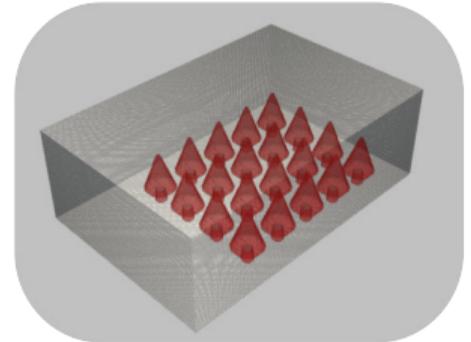
- Acoustic propagation in forest environments



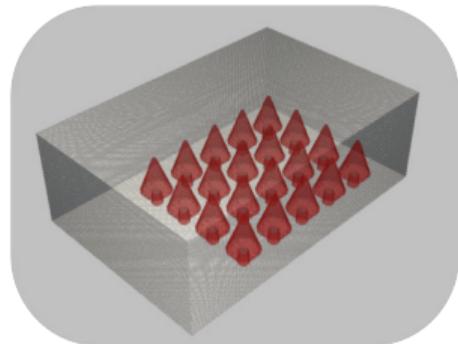
- Acoustic propagation in forest environments
 - Multi-scale
 - Multiple scatterers
 - Impedance boundary conditions



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- Various sources



- Acoustic propagation in forest environments
 - Multi-scale
 - Multiple scatterers
 - Impedance boundary conditions
- Various sources
- European directive [2002/49/EC]: protection of quiet areas



History

Transmission Line Matrix model (TLM)

Introduced to model high frequency magnetic fields
[Johns and Beurle, 1971].

- Time-domain method

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 - Propagation in urban areas [Guillaume et al., 2008]
 - Propagation through parallel cylinders above a horizontal plane [ChobEAU et al., 2017]

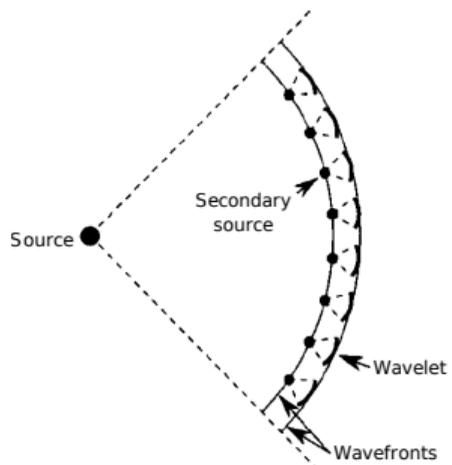
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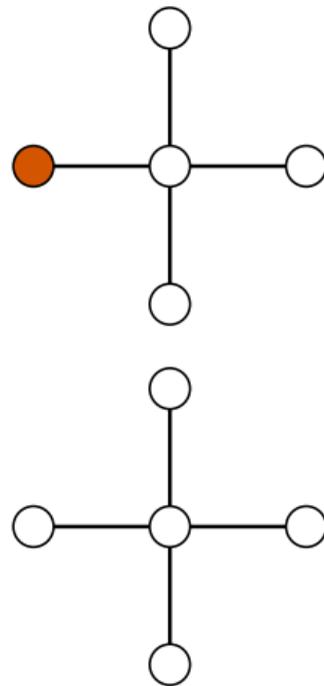
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- Python/OpenCL parallelized on GPUs [Guillaume and Fortin, 2014]

Basis

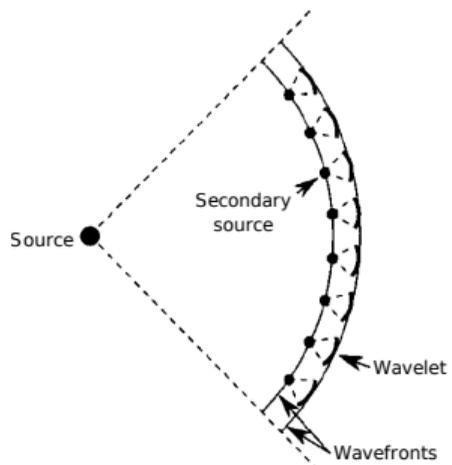


Huygens principle [Guillaume, 2009].

(+) detailed : [Goestchel et al., 2022]

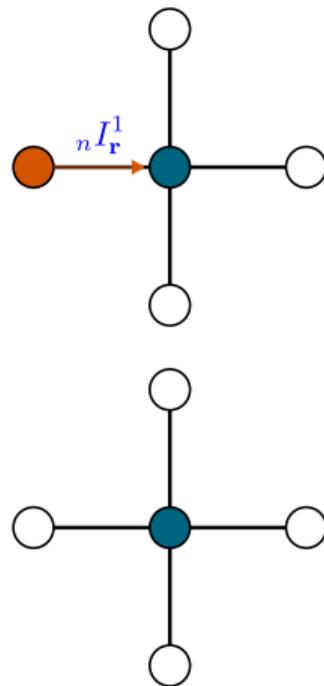


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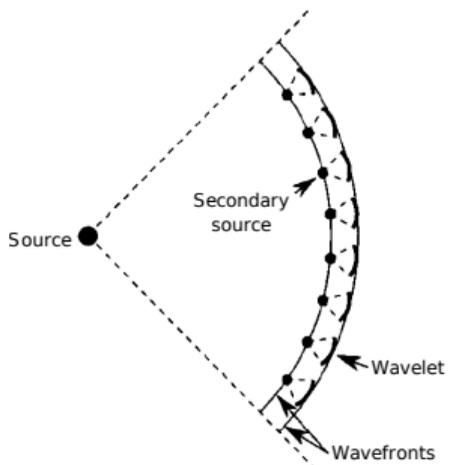


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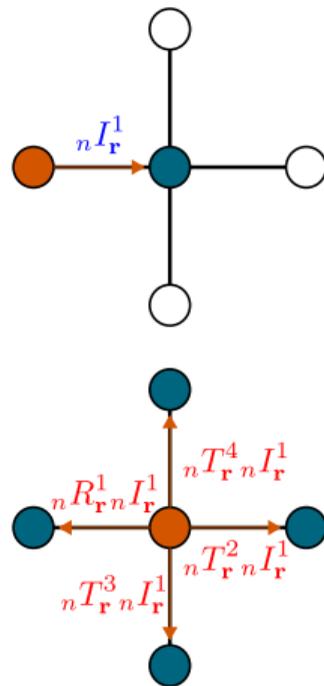


Basis



Huygens principle [Guillaume, 2009].

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Stability study

Homogeneous case

$${}_{n+1}P_{\mathbf{r}} + {}_{n-1}P_{\mathbf{r}} = \frac{1}{d} \sum_{m=1}^d \left[{}_n P_{(j_1+\delta_{m1}, \dots, j_d+\delta_{md})} + {}_n P_{(j_1-\delta_{m1}, \dots, j_d-\delta_{md})} \right], \quad (1)$$

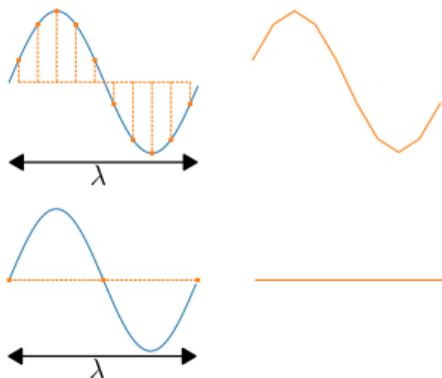
$$\frac{\partial^2 p}{\partial t^2} - c_{\text{TLM}}^2 \nabla^2 p = \mathcal{O}(\Delta t^2) + \mathcal{O}\left(\frac{\Delta \ell^4}{\Delta t^2}\right), \quad \text{with } c_{\text{TLM}} = \frac{\Delta \ell}{\sqrt{d} \Delta t}. \quad (2)$$

Axial dispersion

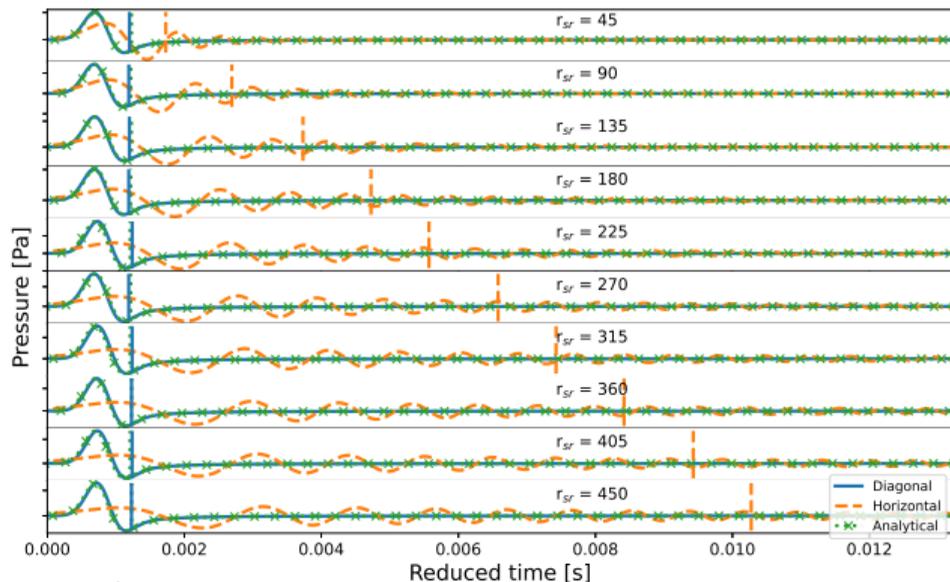
$$\cos(\omega \Delta t) = \frac{1}{d} \sum_{m=1}^d \cos(k_{x_m} \Delta \ell) \quad \forall \Delta t, \quad \forall \Delta \ell. \quad (3)$$

Dispersion effect on results

Number of points per wavelength (N_{ppw})

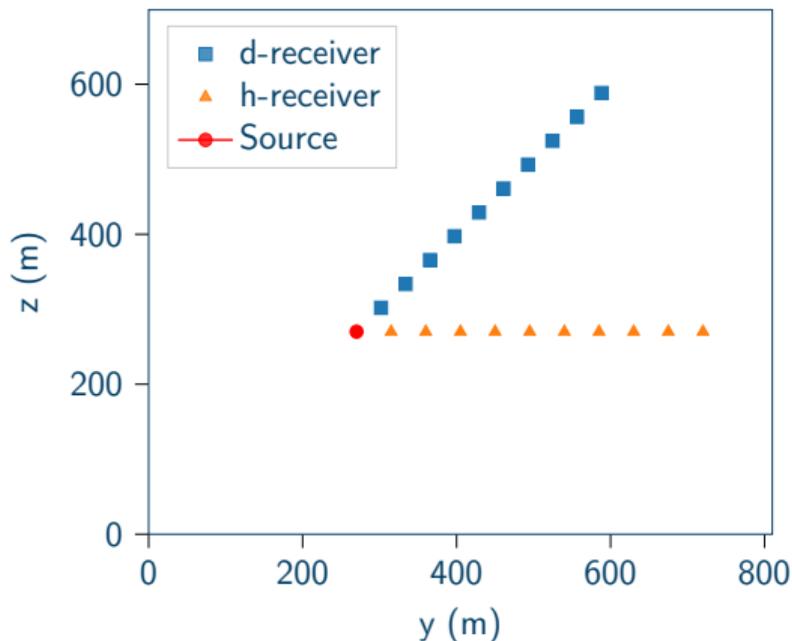


Cartesian mesh numerical dispersion



Free field setup

Calculation domain

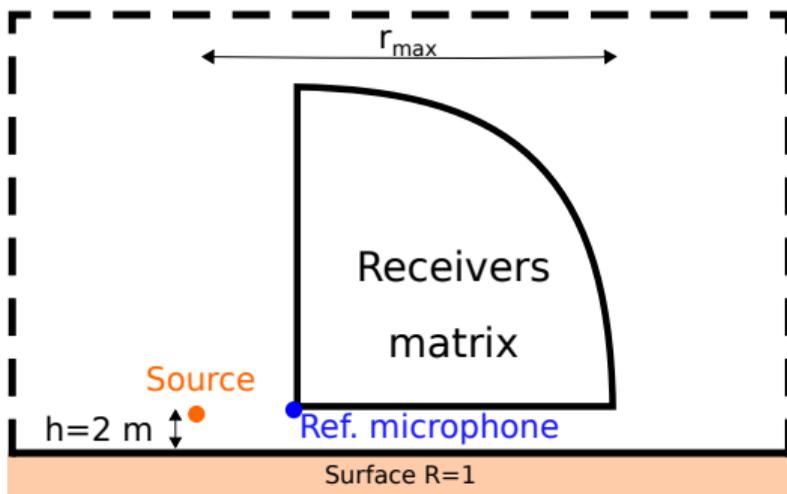


Configuration for $f_{\max} = 2400$ Hz,
 $\Delta\ell = \lambda/10$, $r_{\max} = 450$ m:

$\Delta\ell$ [m]	Δt [s]	$\Delta\ell_{\text{mic}}$ [m]	$N_y \times N_z$ [-]
0.014	2.95E-05	45	56476*48746

Memory [Gb] (float32 numpy array)	t_{sim} [s]	r_{\max}/λ_{\min} [-]
10.22	11143	3176

Reflective ground setup



Normalisation & results

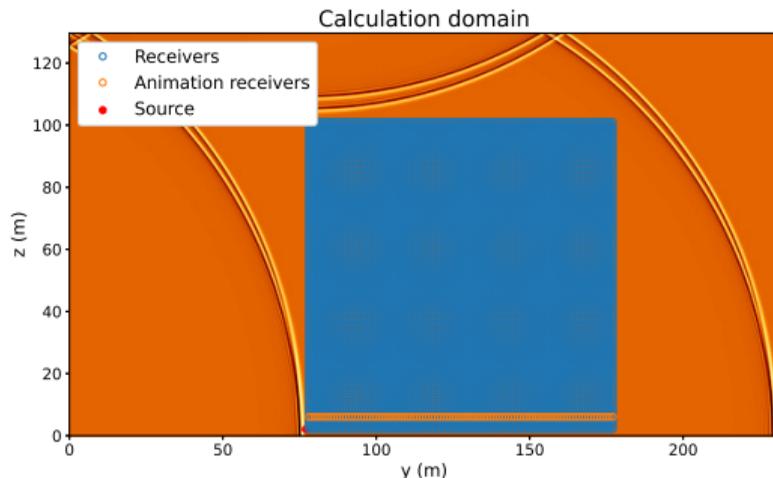
- Normalisation: standard deviation ratio

$$m_{ij}^n = \frac{m_{ij}^n \times \sigma(p_{0j}^n)}{\sigma(m_{0j}^n)}$$

- Attenuation // reference microphone:

$$Att(r) = 10 \times \log \left(\frac{\sum_n p_{ij}^2[n]}{\sum_n p_{0j}^2[n]} \right)$$

Reflective ground setup



Normalisation & results

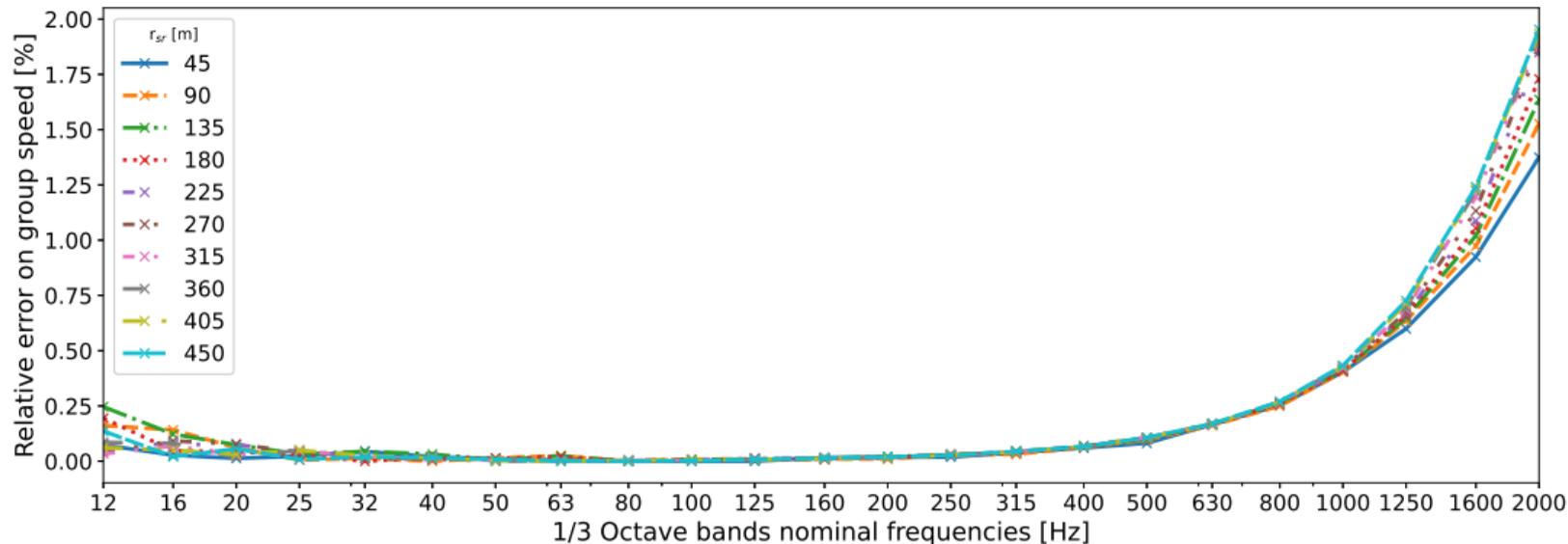
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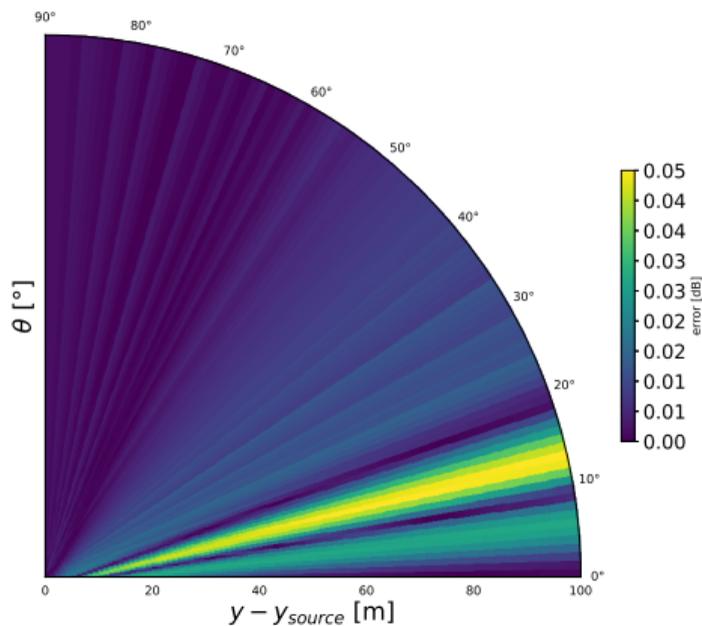
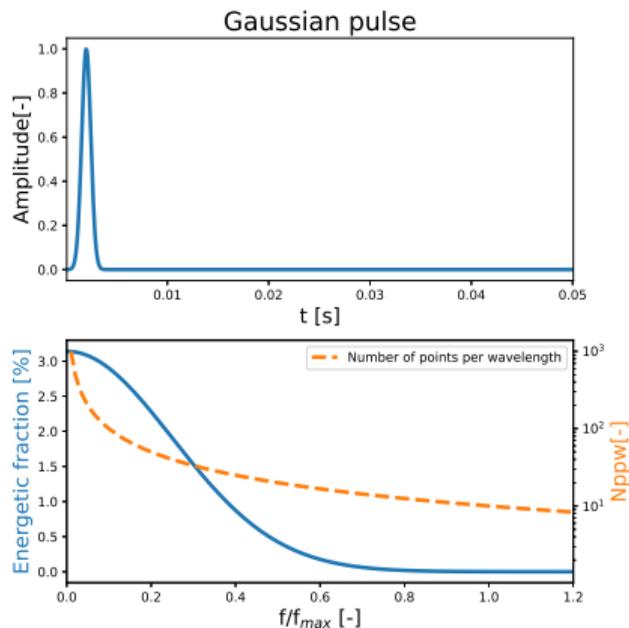
$$Att(r) = 10 \times \log \left(\frac{\sum p_{ij}^2[n]}{n} \right) / \left(\frac{\sum p_{0j}^2[n]}{n} \right)$$

Free Field - pulse

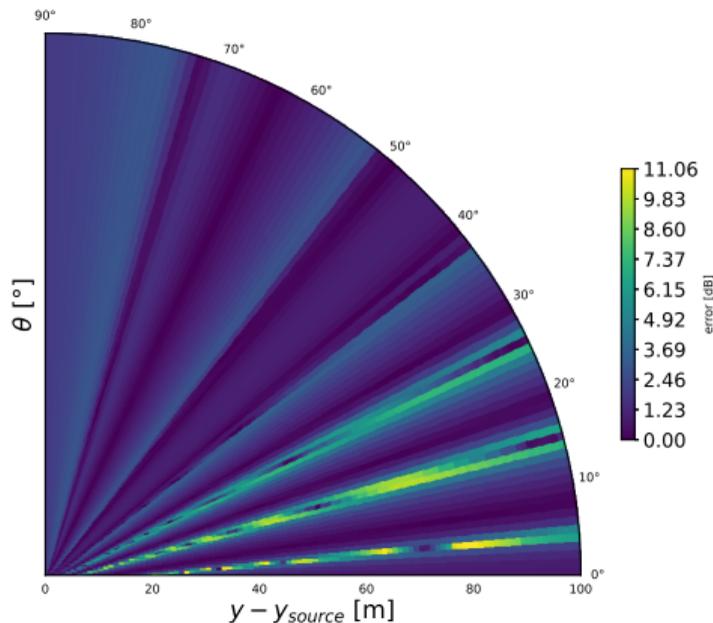
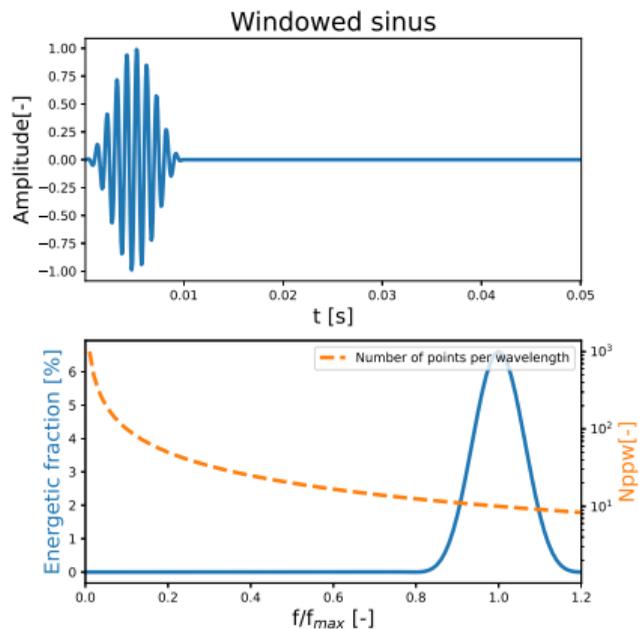


Error on group speed, $\Delta\ell = \lambda/10$, $f_{\max} = 2400$ Hz.

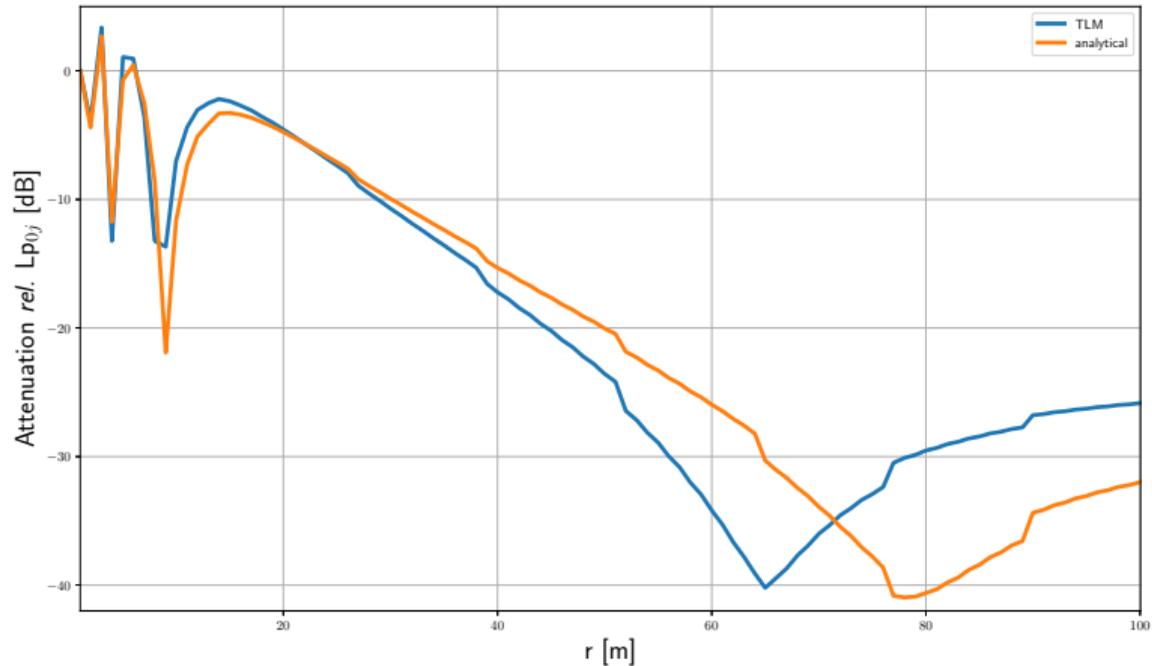
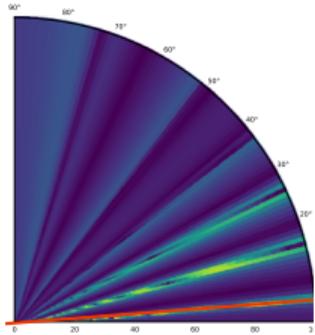
Ground reflection - pulse



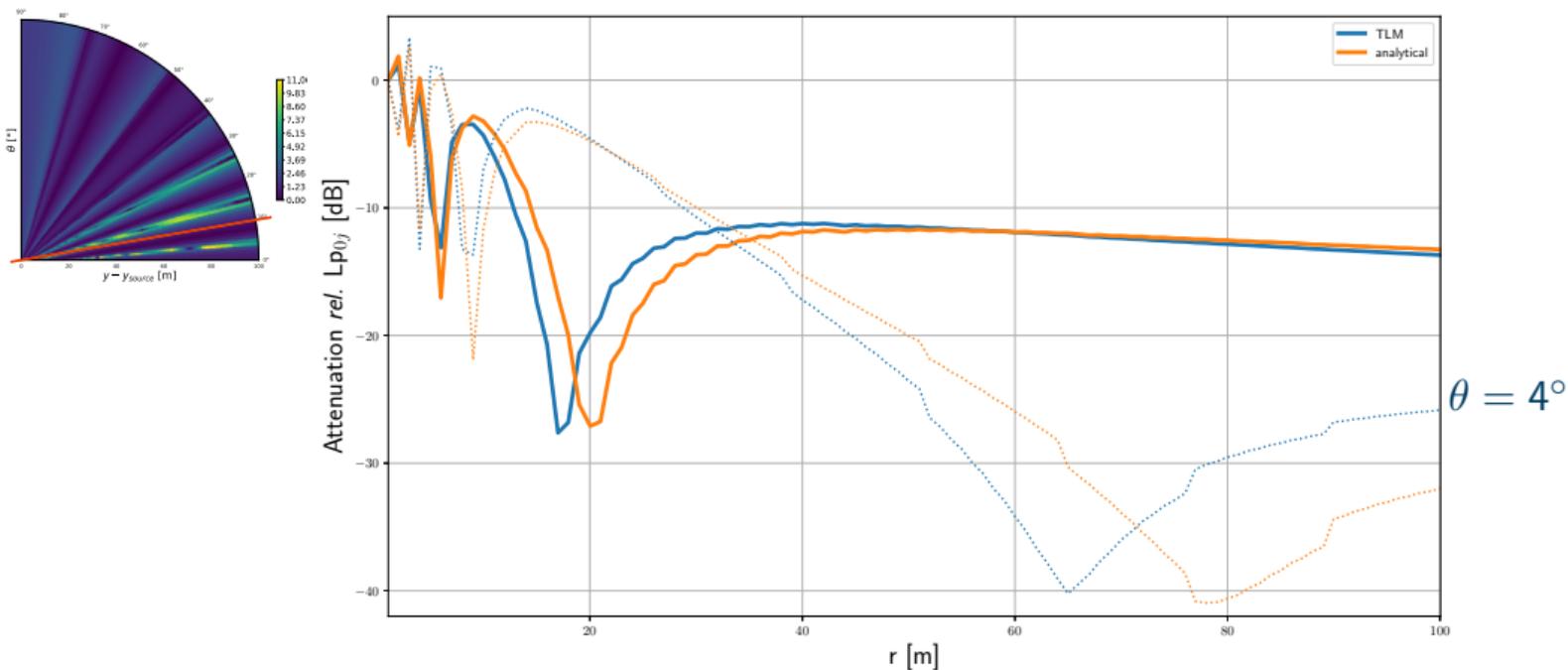
Ground reflection - windowed sinus



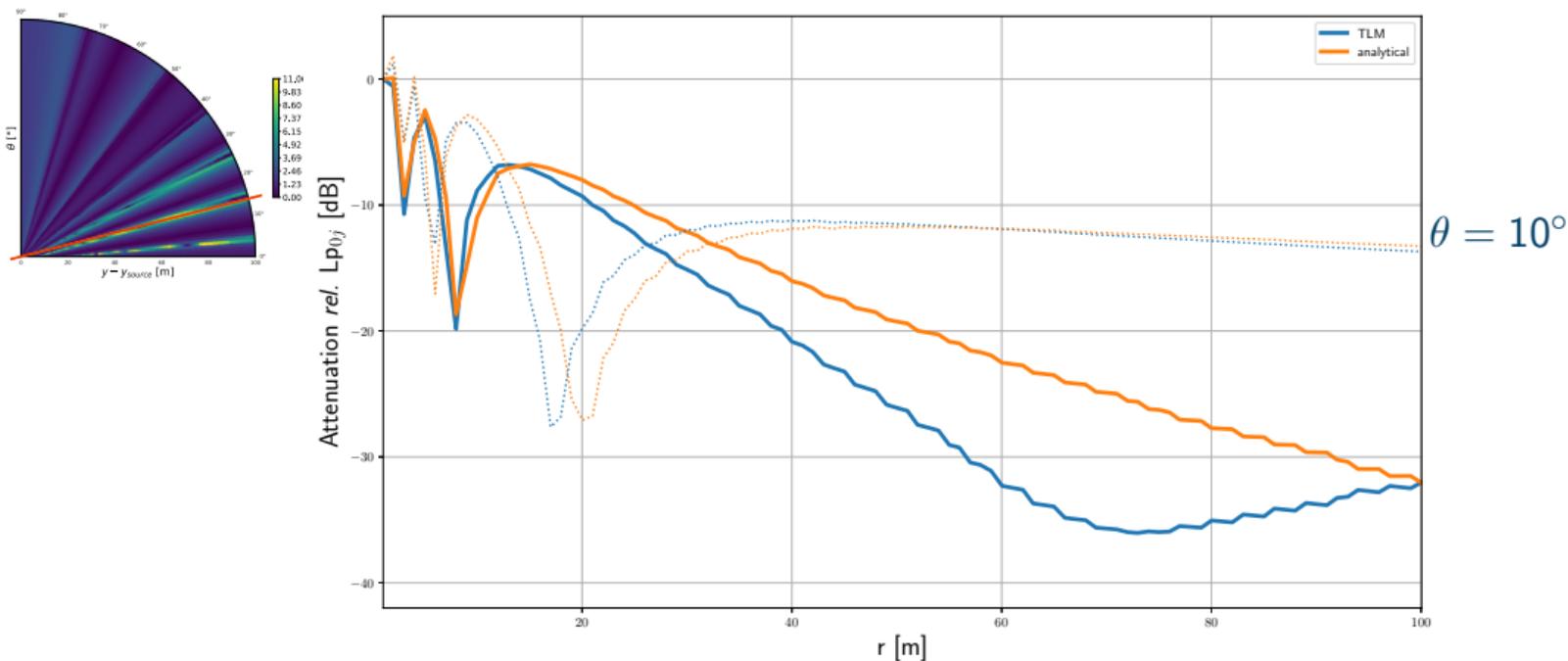
Ground reflection - windowed sinus, $\theta = 4^\circ$



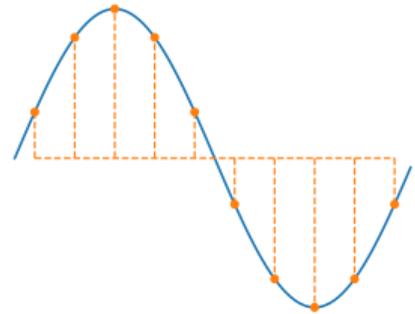
Ground reflection - windowed sinus, $\theta = 10^\circ$



Ground reflection - windowed sinus, $\theta = 15^\circ$

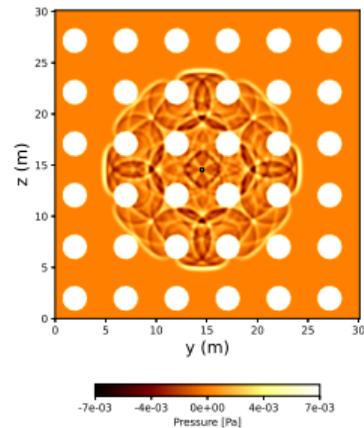
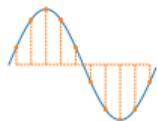


- 10 points per wavelength criterion not sufficient



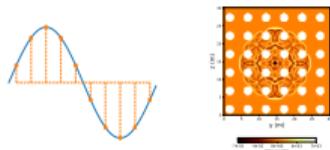
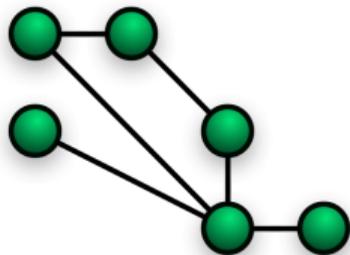
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- Compare complex modelling with measurements



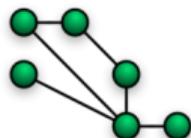
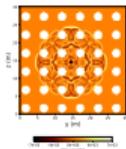
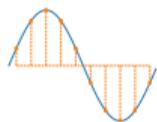
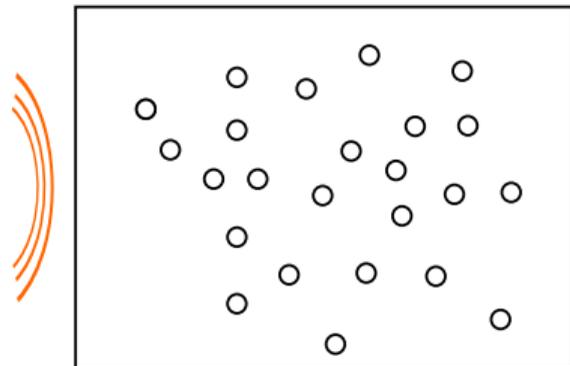
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- Compare complex modelling with measurements
- Increase the scheme order or change?



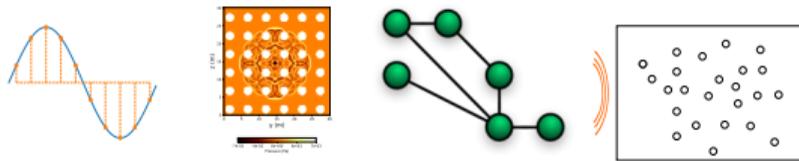
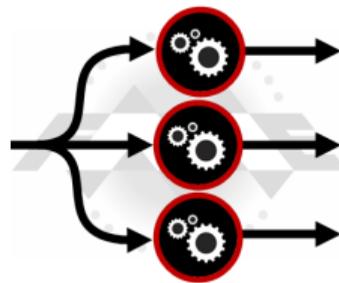
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- Waves in complex media theory



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- Compare complex modelling with measurements
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- Waves in complex media theory
- MPI parallelization



- 
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A Transmission Line Matrix model for sound propagation in arrays of cylinders normal to an impedance plane.
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Journal of Sound and Vibration, 531:116974.
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PhD thesis.
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Journal of Building Performance Simulation, 7(6):445–456.
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Use of the transmission line matrix method for the sound propagation modeling in urban area.
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Numerical solution of 2-dimensional scattering problems using a transmission-line matrix.
Proceedings of the Institution of Electrical Engineers, 118(9):1203–1203.

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- links :
 - <http://www.umrae.fr/>

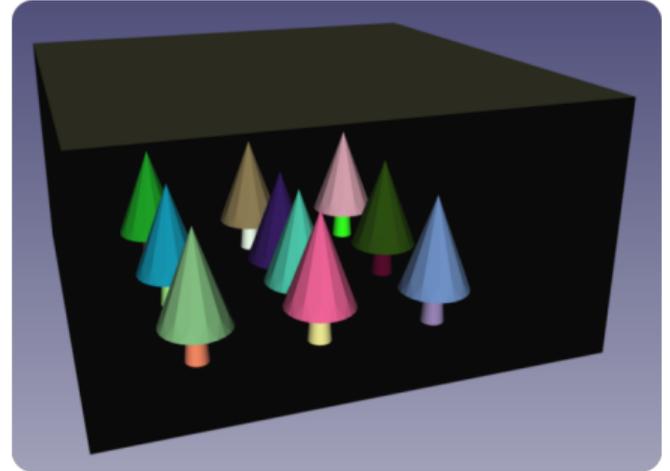


Unité Mixte de Recherche en Acoustique Environnementale (UMRAE) is a joint research unit in environmental acoustics between Gustave Eiffel University & Cerema.

Appendix

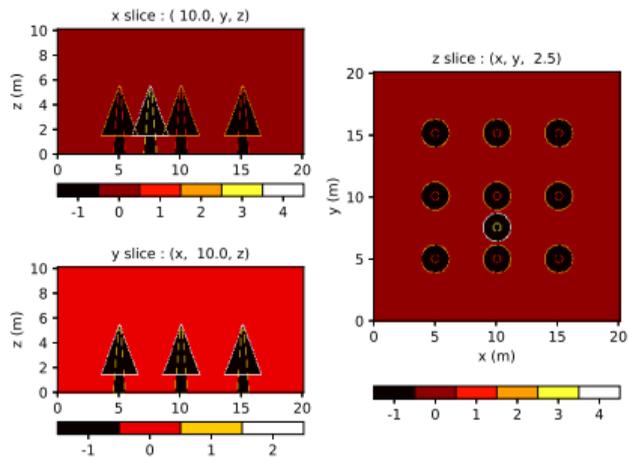
Meshing & implementation

- FreeCAD API automatic scene generation
 - (Supervision of an IT student's internship)



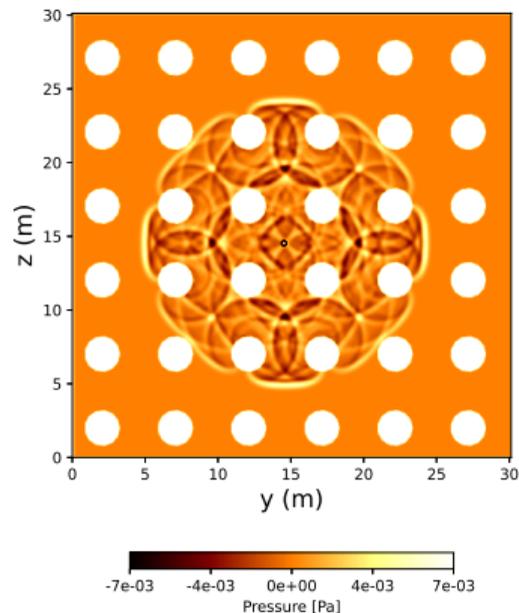
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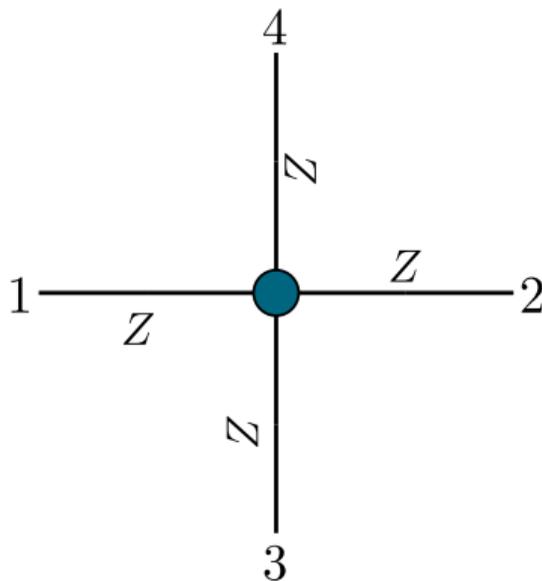
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- Fast voxelization process
<https://github.com/nicolas-f/FastVoxel>



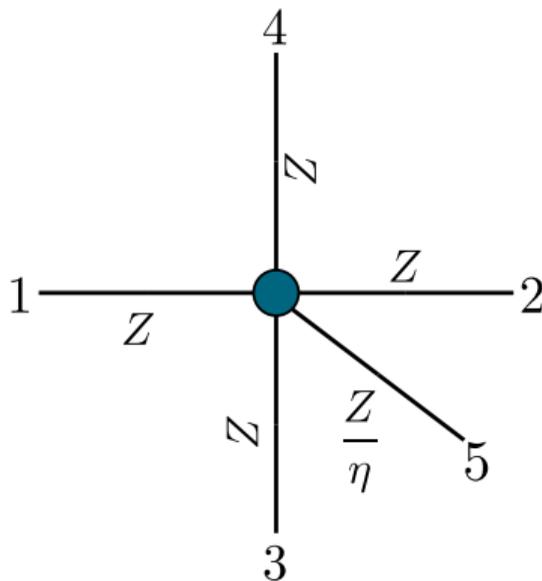
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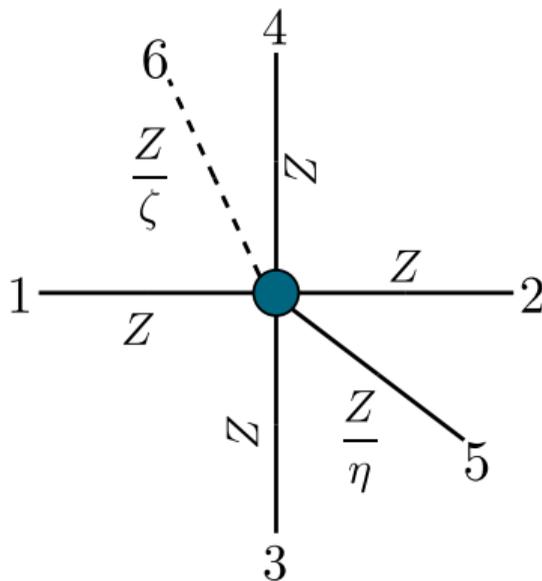




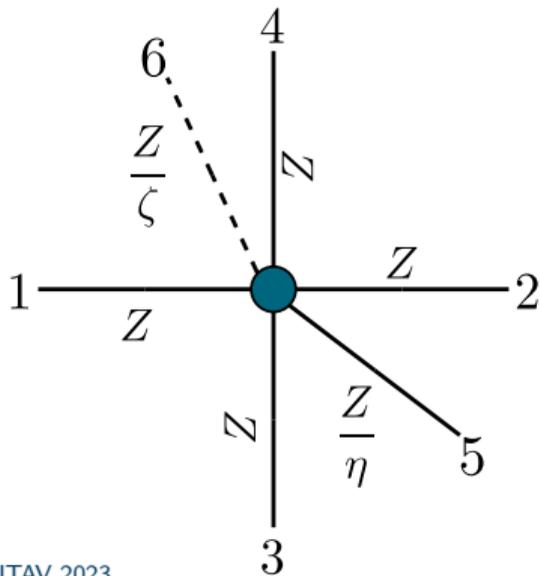
2D stencil around a node



2D stencil around a node



2D stencil around a node



Link to wave equation

$$\frac{1}{c_{\text{TLM}}^2} \frac{\partial^2 p}{\partial t^2} - \nabla^2 p + \frac{\zeta_{(j,l)}}{2\Delta\ell^2} \left(2\Delta t \frac{\partial p}{\partial t} \right) = \mathcal{O} \left(\frac{\Delta t^4}{\Delta\ell^2} \right) + \mathcal{O} \left(\frac{\Delta t^3}{\Delta\ell^2} \right) + \mathcal{O} \left(\Delta\ell^2 \right) \quad (4)$$

Stability

$$c_{\text{TLM}}(\mathbf{x}_r) = \sqrt{\frac{2}{\eta_r + 2d} \frac{\Delta \ell}{\Delta t}} \quad (5)$$

$$\eta \geq 0$$

Dispersion

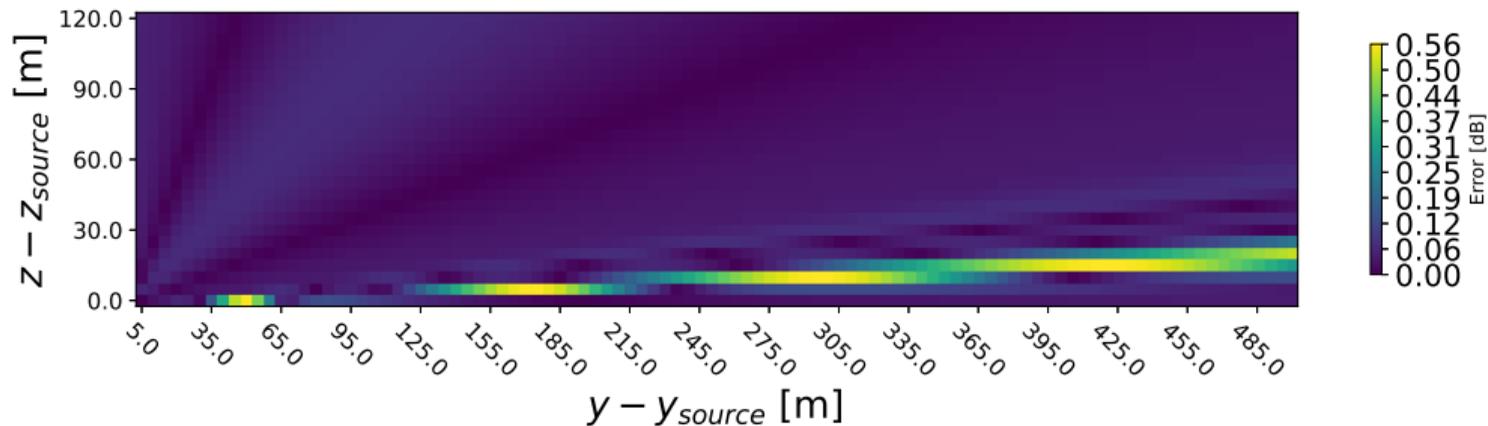
$$\|\underline{k}\| \approx k_{0\text{TLM}} + i\alpha_{\text{TLM}} + \mathcal{O}(\zeta^2) \quad (6)$$

$$k_{0\text{TLM}} = \frac{\omega}{c_{\text{TLM}}} \text{ and}$$

$$\alpha_{\text{TLM}} = \frac{\zeta}{\sqrt{2(\eta + 2d)} \Delta \ell}$$

Ground reflection : Richer Wavelet

Error map: $f_{\max} = 2000$ Hz, $r_{\max} = 500$ m et $h_{\text{src}} = 2$ m



Ground reflection : windowed sinus

Error map: $f_{\max} = 2000$ Hz, $r_{\max} = 500$ m et $h_{\text{src}} = 2$ m

